

**Table 5.1** Summary of penalty parameters' settings applied to different problems constituted for various types of riprap stones

| Optimization Algorithm      | Type of Riprap Stones ( $\phi$ ) | Objective Function | Manning's Roughness Coefficient for Channel Bed, $n_b$ | Values of constant ' $a_1$ ' and ' $a_2$ ' in Eq. 5.5 |              |              | Inertia weight, $\omega$ | Maximum Number of Iterations | Flow Rate and Stone Stability Constraint Equations | Freeboard Scenarios                              |
|-----------------------------|----------------------------------|--------------------|--------------------------------------------------------|-------------------------------------------------------|--------------|--------------|--------------------------|------------------------------|----------------------------------------------------|--------------------------------------------------|
|                             |                                  |                    |                                                        | $j = 1$                                               | $j = 2$      | $j = 3$      |                          |                              |                                                    |                                                  |
| Particle Swarm Optimization | Round (31.8 °)                   | Model 1            | 0.025                                                  | 1.410, 0.315                                          | 1.200, 0.340 | 1.100, 0.340 | 0.50-0                   | 100                          | Eqs. 3.59-3.61                                     | <i>Scenario 1</i><br>$f = 0$                     |
|                             |                                  |                    | Using Eq. 3.35                                         | 1.410, 0.315                                          | 1.200, 0.440 | 1.100, 0.340 | 0.83-0                   |                              |                                                    | <i>Scenario 2</i><br>$f = 0.5$                   |
|                             | Subround and subangular (34.6 °) | Model 2            | 0.025                                                  | 1.040, 1.000                                          | 0.700, 0.434 | 1.660, 2.100 | 0.81-0                   |                              |                                                    | <i>Scenario 3</i><br>$f = 0.5\ y^{0.25}$         |
|                             |                                  |                    | Using Eq. 3.35                                         | 0.960, 1.000                                          | 0.620, 1.400 | 1.400, 1.250 | 0.80-0                   |                              |                                                    |                                                  |
|                             | Angular (38.4 °)                 | Model 3            | 0.025                                                  | 0.960, 0.760                                          | 0.760, 0.760 | 0.960, 0.430 | 0.688-0                  | 220                          |                                                    | <i>Scenario 4</i><br>$f = 0.25 + 0.25\ y^{0.25}$ |
|                             |                                  |                    | Using Eq. 3.35                                         | 0.960, 0.760                                          | 0.760, 0.760 | 0.960, 0.430 | 0.688-0                  |                              |                                                    | <i>Scenario 5</i><br>$f = 0.25 + 0.25\ y^{0.5}$  |

**Table 5.2** Summary of the adopted ranges of decision variables

| S. No. | Angle of repose, $\phi(^{\circ})$ | Bottom width of canal, $b$ (m) | Depth of flow, $y$ (m) | Canal side slope, $m_1(H): 1(V)$ | Canal side slope, $m_2(H): 1(V)$ | Size of riprap stone, $D$ (m) |
|--------|-----------------------------------|--------------------------------|------------------------|----------------------------------|----------------------------------|-------------------------------|
| 1      | 31.8                              | 2.5-15.0                       | 0.5-5.0                | 1.613-3.0                        | 1.613-3.0                        | 0.1-1.0                       |
| 2      | 34.6                              | 2.5-15.0                       | 0.5-5.0                | 1.450-3.0                        | 1.45-3.0                         | 0.1-1.0                       |
| 3      | 38.4                              | 2.5-15.0                       | 0.5-5.0                | 1.262-3.0                        | 1.262-3.0                        | 0.1-1.0                       |

**Table 5.3** Least cost canal characteristics obtained by application of Particle Swarm Optimization using round riprap stones

| Column Number→        | 1                                                                     | 2                       | 3                      | 4              | 5             | 6                 | 7                 | 8                     | 9             | 10                          | 11                   | 12            | 13           | 14                  | 15                       | 16                              | 17                              | 18                     | 19                 |
|-----------------------|-----------------------------------------------------------------------|-------------------------|------------------------|----------------|---------------|-------------------|-------------------|-----------------------|---------------|-----------------------------|----------------------|---------------|--------------|---------------------|--------------------------|---------------------------------|---------------------------------|------------------------|--------------------|
| Row Number for Case I | Freeboard scenarios                                                   | Angle of Repose $\phi$  | Canal bottom width $b$ | Flow depth $y$ | Freeboard $f$ | Side slope, $m_1$ | Side slope, $m_2$ | Riprap stone size $D$ | Top Width $T$ | Side slopes perimeter $P_s$ | Excavated area $A_i$ | Discharge $Q$ | Velocity $V$ | Froude Number, $Fr$ | Cost of construction $C$ | Residual <i>LHS of Eq. 3.47</i> | Residual <i>LHS of Eq. 3.48</i> | Residual $R_1+R_2+R_3$ | Basis of Selection |
|                       | Case I: Clear water flow near channel bed ( $n_b = 0.025$ )           |                         |                        |                |               |                   |                   |                       |               |                             |                      |               |              |                     |                          |                                 |                                 |                        |                    |
|                       | 1                                                                     | $k=0$<br>$C=0$<br>$x=0$ | 31.8                   | 7.7399         | 3.0878        | 0.0000            | 1.8385            | 1.8385                | 0.1249        | 19.0940                     | 12.9250              | 41.4290       | 59.9996      | 1.4483              | 0.2632                   | 321.3464                        | 0.0010                          | 0.0000                 | 0.0000             |
| 2                     | $k=0.5$<br>$C=0$<br>$x=0$                                             | 31.8                    | 7.7239                 | 3.0935         | 0.5000        | 1.8306            | 1.8306            | 0.1272                | 20.8803       | 14.9915                     | 51.3951              | 60.0000       | 1.4488       | 0.2630              | 384.8030                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 3                     | $k=0$<br>$C=0.5$<br>$x=0.25$                                          | 31.8                    | 7.7239                 | 3.0935         | 0.6631        | 1.8306            | 1.8306            | 0.1272                | 21.4774       | 15.6719                     | 54.8495              | 59.9999       | 1.4488       | 0.2630              | 405.8179                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 4                     | $k=0.25$<br>$C=0.25$<br>$x=0.25$                                      | 31.8                    | 7.7239                 | 3.0935         | 0.5816        | 1.8306            | 1.8306            | 0.1272                | 21.1789       | 15.3317                     | 53.1101              | 60.0000       | 1.4488       | 0.2630              | 395.2612                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 5                     | $k=0.25$<br>$C=0.25$<br>$x=0.5$                                       | 31.8                    | 7.7239                 | 3.0935         | 0.6897        | 1.8306            | 1.8306            | 0.1272                | 21.5748       | 15.7829                     | 55.4221              | 59.9999       | 1.4488       | 0.2630              | 409.2831                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| Row Number for CaseII | Case II: Sediment laden flow near channel bottom ( $n_b$ using Eq. 3) |                         |                        |                |               |                   |                   |                       |               |                             |                      |               |              |                     |                          |                                 |                                 |                        |                    |
| 1                     | $k=0$<br>$C=0$<br>$x=0$                                               | 31.8                    | 10.0292                | 2.6124         | 0.0000        | 1.8680            | 1.8680            | 0.1076                | 19.7892       | 11.0705                     | 38.9490              | 60.1903       | 1.5454       | 0.3053              | 287.2650                 | 0.0009                          | 0.0030                          | 0.0033                 | GM and MR both     |
| 2                     | $k=0.5$<br>$C=0$<br>$x=0$                                             | 31.8                    | 8.3898                 | 2.8416         | 0.5000        | 1.8272            | 1.8272            | 0.1250                | 20.6013       | 13.9208                     | 48.4390              | 60.0000       | 1.5546       | 0.2945              | 361.7991                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 3                     | $k=0$<br>$C=0.5$<br>$x=0.25$                                          | 31.8                    | 8.3898                 | 2.8416         | 0.6492        | 1.8272            | 1.8272            | 0.1250                | 21.1465       | 14.5422                     | 51.5528              | 60.0000       | 1.5546       | 0.2945              | 380.7424                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 4                     | $k=0.25$<br>$C=0.25$<br>$x=0.25$                                      | 31.8                    | 8.3898                 | 2.8416         | 0.5746        | 1.8272            | 1.8272            | 0.1250                | 20.8739       | 14.2314                     | 49.9857              | 60.0000       | 1.5546       | 0.2945              | 371.2298                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 5                     | $k=0.25$<br>$C=0.25$<br>$x=0.5$                                       | 31.8                    | 8.3993                 | 2.8405         | 0.6713        | 1.8263            | 1.8263            | 0.1252                | 21.2267       | 14.6245                     | 52.0204              | 60.0000       | 1.5547       | 0.2946              | 383.6724                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |

**GM:** The best solution selected based on the global minimum cost; **MR:** The best solution obtained based on the minimum sum of all residuals ( $R_1+R_2+R_3$ )

**Table 5.4** Least cost canal characteristics obtained by application of Particle Swarm Optimization with subround and subangular stones

| Column Number<br>→    | 1                                                                     | 2                      | 3                      | 4              | 5             | 6                 | 7                 | 8                     | 9             | 10                          | 11                   | 12            | 13           | 14                  | 15                       | 16                              | 17                              | 18                     | 19                 |
|-----------------------|-----------------------------------------------------------------------|------------------------|------------------------|----------------|---------------|-------------------|-------------------|-----------------------|---------------|-----------------------------|----------------------|---------------|--------------|---------------------|--------------------------|---------------------------------|---------------------------------|------------------------|--------------------|
| Row Number for Case I | Freeboard scenarios                                                   | Angle of Repose $\phi$ | Canal bottom width $b$ | Flow depth $y$ | Freeboard $f$ | Side slope, $m_1$ | Side slope, $m_2$ | Riprap stone size $D$ | Top Width $T$ | Side slopes perimeter $P_s$ | Excavated area $A_t$ | Discharge $Q$ | Velocity $V$ | Froude Number, $Fr$ | Cost of construction $C$ | Actual Residual LHS of Eq. 3.47 | Actual Residual LHS of Eq. 3.48 | Residual $R_1+R_2+R_3$ | Basis of Selection |
|                       | Case I: Clear water flow near channel bed ( $n_b = 0.025$ )           |                        |                        |                |               |                   |                   |                       |               |                             |                      |               |              |                     |                          |                                 |                                 |                        |                    |
| 1                     | $k=0$<br>$C=0$<br>$x=0$                                               | 34.6                   | 8.3532                 | 3.0396         | 0.0000        | 1.6419            | 1.6418            | 0.1156                | 18.3341       | 11.6865                     | 40.5591              | 60.1421       | 1.4828       | 0.2716              | 290.5600                 | 0.0037                          | -0.0025                         | 0.0026                 | GM and MR both     |
| 2                     | $k=0.5$<br>$C=0$<br>$x=0$                                             | 34.6                   | 8.3697                 | 3.0335         | 0.5000        | 1.6401            | 1.6404            | 0.1157                | 19.9611       | 13.5758                     | 50.0533              | 59.9933       | 1.4819       | 0.2717              | 345.7464                 | -0.0264                         | -0.0074                         | 0.0015                 |                    |
| 3                     | $k=0$<br>$C=0.5$<br>$x=0.25$                                          | 34.6                   | 8.3697                 | 3.0335         | 0.6599        | 1.6401            | 1.6404            | 0.1157                | 20.4855       | 14.1900                     | 53.2863              | 59.9933       | 1.4819       | 0.2717              | 364.2377                 | -0.0264                         | -0.0074                         | 0.0015                 |                    |
| 4                     | $k=0.25$<br>$C=0.25$<br>$x=0.25$                                      | 34.6                   | 8.3697                 | 3.0335         | 0.5799        | 1.6401            | 1.6404            | 0.1157                | 20.2233       | 13.8829                     | 51.6593              | 59.9933       | 1.4819       | 0.2717              | 354.9496                 | -0.0264                         | -0.0074                         | 0.0015                 |                    |
| 5                     | $k=0.25$<br>$C=0.25$<br>$x=0.5$                                       | 34.6                   | 8.3697                 | 3.0335         | 0.6854        | 1.6401            | 1.6404            | 0.1157                | 20.5694       | 14.2882                     | 53.8109              | 59.9933       | 1.4819       | 0.2717              | 367.2254                 | -0.0264                         | -0.0074                         | 0.0015                 |                    |
| Row Number for CaseII | Case II: Sediment laden flow near channel bottom ( $n_b$ using Eq. 3) |                        |                        |                |               |                   |                   |                       |               |                             |                      |               |              |                     |                          |                                 |                                 |                        |                    |
| 1                     | $k=0$<br>$C=0$<br>$x=0$                                               | 34.6                   | 6.3596                 | 3.2353         | 0.0000        | 1.6513            | 1.6513            | 0.1224                | 17.0445       | 12.4915                     | 37.8596              | 59.9999       | 1.5848       | 0.2814              | 285.7810                 | 0.0000                          | 0.0000                          | 0.0000                 | GM and MR both     |
| 2                     | $k=0.5$<br>$C=0$<br>$x=0$                                             | 34.6                   | 6.3729                 | 3.2318         | 0.5000        | 1.6528            | 1.6528            | 0.1219                | 18.7090       | 14.4182                     | 46.8003              | 60.0001       | 1.5848       | 0.2815              | 339.2825                 | 0.0000                          | 0.0001                          | 0.0000                 |                    |
| 3                     | $k=0$<br>$C=0.5$<br>$x=0.25$                                          | 34.6                   | 6.5740                 | 3.1904         | 0.6682        | 1.6504            | 1.6504            | 0.1217                | 19.3107       | 14.8922                     | 49.9391              | 59.9645       | 1.5875       | 0.2838              | 356.6866                 | 0.0004                          | -0.0005                         | 0.0006                 |                    |
| 4                     | $k=0.25$<br>$C=0.25$<br>$x=0.25$                                      | 34.6                   | 6.3729                 | 3.2318         | 0.5852        | 1.6528            | 1.6528            | 0.1219                | 18.9906       | 14.7474                     | 48.4062              | 60.0001       | 1.5848       | 0.2815              | 348.7931                 | 0.0000                          | 0.0001                          | 0.0000                 |                    |
| 5                     | $k=0.25$<br>$C=0.25$<br>$x=0.5$                                       | 34.6                   | 6.5740                 | 3.1904         | 0.6965        | 1.6504            | 1.6504            | 0.1217                | 19.4041       | 15.0015                     | 50.4870              | 59.9645       | 1.5875       | 0.2838              | 359.9017                 | 0.0004                          | -0.0005                         | 0.0006                 |                    |

**Table 5.5** Least cost canal characteristics obtained by application of Particle Swarm Optimization with angular riprap stones

| Column Number→         | 1                                                                     | 2                      | 3                      | 4              | 5            | 6                 | 7                 | 8                     | 9             | 10                          | 11                   | 12            | 13           | 14                  | 15                       | 16                              | 17                              | 18                     | 19                 |
|------------------------|-----------------------------------------------------------------------|------------------------|------------------------|----------------|--------------|-------------------|-------------------|-----------------------|---------------|-----------------------------|----------------------|---------------|--------------|---------------------|--------------------------|---------------------------------|---------------------------------|------------------------|--------------------|
| Row Number for Case I  | Freeboard scenarios                                                   | Angle of Repose $\phi$ | Canal bottom width $b$ | Flow depth $y$ | Freeboad $f$ | Side slope, $m_1$ | Side slope, $m_2$ | Riprap stone size $D$ | Top Width $T$ | Side slopes perimeter $P_s$ | Excavated area $A_t$ | Discharge $Q$ | Velocity $V$ | Froude Number, $Fr$ | Cost of construction $C$ | Residual <i>LHS of Eq. 3.47</i> | Residual <i>LHS of Eq. 3.48</i> | Residual $R_1+R_2+R_3$ | Basis of Selection |
|                        | Case I: Clear water flow near channel bed ( $n_b = 0.025$ )           |                        |                        |                |              |                   |                   |                       |               |                             |                      |               |              |                     |                          |                                 |                                 |                        |                    |
| 1                      | $k=0$<br>$C=0$<br>$x=0$                                               | 38.4                   | 8.6154                 | 3.0655         | 0.0000       | 1.3739            | 1.3739            | 0.1266                | 17.0385       | 10.4181                     | 39.3207              | 59.9999       | 1.5259       | 0.2783              | 269.8180                 | 0.0000                          | 0.0000                          | 0.0000                 | GM and MR both     |
| 2                      | $k=0.5$<br>$C=0$<br>$x=0$                                             | 38.4                   | 8.6138                 | 3.0661         | 0.5000       | 1.3730            | 1.3730            | 0.1271                | 18.4066       | 12.1148                     | 48.1791              | 59.9999       | 1.5260       | 0.2783              | 320.0014                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 3                      | $k=0$<br>$C=0.5$<br>$x=0.25$                                          | 38.4                   | 8.6138                 | 3.0661         | 0.6616       | 1.3730            | 1.3730            | 0.1271                | 18.8504       | 12.6639                     | 51.1901              | 59.9999       | 1.5260       | 0.2783              | 336.7488                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 4                      | $k=0.25$<br>$C=0.25$<br>$x=0.25$                                      | 38.4                   | 8.6138                 | 3.0661         | 0.5808       | 1.3730            | 1.3730            | 0.1271                | 18.6285       | 12.3893                     | 49.6756              | 59.9999       | 1.5260       | 0.2783              | 328.3388                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 5                      | $k=0.25$<br>$C=0.25$<br>$x=0.5$                                       | 38.4                   | 8.6138                 | 3.0661         | 0.6878       | 1.3730            | 1.3730            | 0.1271                | 18.9222       | 12.7526                     | 51.6835              | 59.9999       | 1.5260       | 0.2783              | 339.4830                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| Row Number for Case II | Case II: Sediment laden flow near channel bottom ( $n_b$ using Eq. 3) |                        |                        |                |              |                   |                   |                       |               |                             |                      |               |              |                     |                          |                                 |                                 |                        |                    |
| 1                      | $k=0$<br>$C=0$<br>$x=0$                                               | 38.4                   | 6.8982                 | 3.1960         | 0.0000       | 1.3937            | 1.3937            | 0.1260                | 15.8069       | 10.9647                     | 36.2829              | 59.9999       | 1.6537       | 0.2954              | 256.9989                 | 0.0000                          | 0.0000                          | 0.0000                 | GM and MR both     |
| 2                      | $k=0.5$<br>$C=0$<br>$x=0$                                             | 38.4                   | 7.9983                 | 2.9996         | 0.5000       | 1.3617            | 1.3617            | 0.1389                | 17.5290       | 11.8247                     | 44.6677              | 59.9999       | 1.6555       | 0.3052              | 308.1187                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 3                      | $k=0$<br>$C=0.5$<br>$x=0.25$                                          | 38.4                   | 8.0898                 | 2.9843         | 0.6572       | 1.3598            | 1.3598            | 0.1397                | 17.9928       | 12.2926                     | 47.4888              | 59.9999       | 1.6551       | 0.3059              | 324.4233                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 4                      | $k=0.25$<br>$C=0.25$<br>$x=0.25$                                      | 38.4                   | 8.1045                 | 2.9815         | 0.5785       | 1.3601            | 1.3601            | 0.1394                | 17.7886       | 12.0198                     | 46.0897              | 59.9999       | 1.6550       | 0.3061              | 316.1790                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |
| 5                      | $k=0.25$<br>$C=0.25$<br>$x=0.5$                                       | 38.4                   | 8.0891                 | 2.9844         | 0.6819       | 1.3598            | 1.3598            | 0.1397                | 18.0597       | 12.3766                     | 47.9340              | 59.9999       | 1.6551       | 0.3059              | 326.9636                 | 0.0000                          | 0.0000                          | 0.0000                 |                    |

**Table 5.6** Performance comparison of different riprap stones for minimum cost channel under *freeboard scenario 4*

| Flow characteristics near channel bottom | Channel features    | Round stone<br>$\phi = 31.8$ | Subround and subangular stone<br>$\phi = 34.6$ | Angular stone<br>$\phi = 38.4$ | Remark                                             | Cost of channels riveted with angular stone under Cases I-II, \$ |
|------------------------------------------|---------------------|------------------------------|------------------------------------------------|--------------------------------|----------------------------------------------------|------------------------------------------------------------------|
| <b>Clear Water (Case I)</b>              | $b$ (m)             | 7.7239                       | 8.3697                                         | 8.6138                         | -                                                  | 328.3388                                                         |
|                                          | $y$ (m)             | 3.0935                       | 3.0335                                         | 3.0661                         | -                                                  |                                                                  |
|                                          | $m$ (-)             | 1.8306                       | 1.6404                                         | 1.3730                         | Steepest slope for angular stone                   |                                                                  |
|                                          | $V$ (m/s)           | 1.4488                       | 1.4819                                         | 1.5260                         | Highest flow velocity with angular stone revetment |                                                                  |
|                                          | Cost (\$) per meter | 395.2612                     | 354.9496                                       | 328.3388                       | Lowest cost by angular stone                       |                                                                  |
| <b>Sediment-laden flow (Case II)</b>     | $b$ (m)             | 8.3898                       | 6.3729                                         | 8.1045                         | -                                                  | 316.1790<br>(Lower than Case I)                                  |
|                                          | $y$ (m)             | 2.8416                       | 3.2318                                         | 2.9815                         | -                                                  |                                                                  |
|                                          | $m$ (-)             | 1.8272                       | 1.6528                                         | 1.3601                         | Steepest slope for angular stone                   |                                                                  |
|                                          | $V$ (m/s)           | 1.5546                       | 1.5848                                         | 1.6550                         | Highest flow velocity with angular stone revetment |                                                                  |
|                                          | Cost (\$) per meter | 371.2298                     | 348.7931                                       | 316.1790                       | Lowest cost by angular stone                       |                                                                  |